

# **CP** Titanium Grade 2

Type Analysis								
Single figures are nominal except where noted.								
Carbon (Maximum)	0.08 %	Titanium	Balance					
Nitrogen (Maximum)	0.03 %	Iron (Maximum)	0.30 %					
Oxygen (Maximum)	0.250 %	Hydrogen (Maximum)	0.015 %					
Other, Total (Maximum)	0.40 %							

\*For ASTM B 348-99 Carbon = 0.08% maximum and ASTM F 67-95 = 0.1% maximum.

"Other, Each" = 0.1% maximum and "Other, Total" = 0.4% maximum values applicable for ASTM B 348-99 only.

## **General Information**

#### Description

Pure titanium undergoes an allotropic transformation from the hexagonal close-packed alpha phase to the body-centered cubic beta phase at a temperature of 882.5°C(1620.5°F).

Commercially pure, or CP, titanium is unalloyed. At service temperature it consists of 100% hcp alpha phase. As a single-phase material, its properties are controlled by chemistry (iron and interstitial impurity elements) and grain size. CP Titanium is classified into Grades 1 through 4 depending on the yield strength and allowable levels of the elements iron, carbon, nitrogen, and oxygen. CP Ti Grade 2 has a minimum yield strength of 275 Mpa (40 ksi), and relatively low levels of impurity elements, which places it between Grades 1 and 3 in terms of strength.

Grade 2 is widely used because it combines excellent formability and moderate strength with superior corrosion resistance. This combination of properties makes CP Grade 2 titanium a candidate for a large variety of chemical and marine as well as aerospace and medical applications.

#### Applications

CP Titanium Grade 2 may be considered in any application where formability and corrosion resistance are important, and strength requirements are moderate. Some examples of aerospace applications have included airframe skins in "warm" areas, ductwork, brackets, and galley equipment. CP Ti Grade 2 has also been widely used in marine and chemical applications such as condensers, evaporators, reaction vessels for chemical processing, tubing and tube headers in desalinization plants, and cryogenic vessels. Other uses have included items such as jigs, baskets, cathodes and starter-sheet blanks for the electroplating industry, and a variety of medical applications.

### **Corrosion Resistance**

The corrosion resistance of CP Ti Grade 2 is based on the presence of a stable, continuous, tightly adherent oxide layer. This layer forms spontaneously and immediately upon exposure to oxygen. If damaged, it re-forms readily as long as there is some source of oxygen (air or moisture) in the environment. In general, the higher the purity of CP Ti, the greater the corrosion resistance. CP Ti Grade 2, with its relatively low impurity levels, has been widely used because it is capable of performing well in many corrosion-critical applications such as marine environments and chemical processing. In seawater, it is fully resistant to corrosion at temperatures up to 315°C (600°F). The possibility of crevice corrosion must be considered, however, and components appropriately designed to avoid tight crevices.

CP Ti Grade 2 is highly resistant to many chemical environments including oxidizing media, alkaline media, organic compounds and acids, aqueous salt solutions, and wet or dry hot gases. It also has sufficient corrosion resistance in liquid metals, nitric acid, mildly reducing acids, and wet chlorine or bromine gas (as long as a minimal amount of oxygen or water is present).

Conditions under which CP Ti Grade 2 is susceptible to corrosion are strongly reducing acids, alkaline peroxide solutions, and molten chloride salts. Crevice corrosion can occur in hot halide or sulfate solutions (>1000 ppm at 75°C or higher), which can be a consideration in marine applications.

CP Ti Grade 2 is fully resistant to stress-corrosion cracking (SCC) in aqueous solutions, and is largely immune to SCC in general. Conditions under which CP Ti Grade 2 is susceptible to SCC include anhydrous methanol or methanol/halide solutions, red fuming nitric acid, nitrous oxide, liquid or solid cadmium and liquid mercury.

CP Grade 2 titanium is susceptible to hydrogen embrittlement due to the formation of hydrides. Specifications for CP Ti Grade 2 mill products typically specify a maximum hydrogen limit of 150 ppm, but it is possible for degradation to occur at lower levels, especially in the presence of a notch. The presence of a notch or other stress raiser increases the detrimental effect, as hydrogen migrates to the notch area, raising the local concentration of hydrides. It is important to minimize hydrogen pickup during processing, particularly heat treating and acid pickling.

**Important Note:** The following 4-level rating scale is intended for comparative purposes only. Corrosion testing is recommended; factors which affect corrosion resistance include temperature, concentration, pH, impurities, aeration, velocity, crevices, deposits, metallurgical condition, stress, surface finish and dissimilar metal contact.

Sulfuric Acid	Moderate	Acetic Acid	Excellent
Sodium Hydroxide	Moderate	Salt Spray (NaCl)	Excellent
Sea Water	Excellent	Sour Oil/Gas	Moderate
Humidity	Excellent		

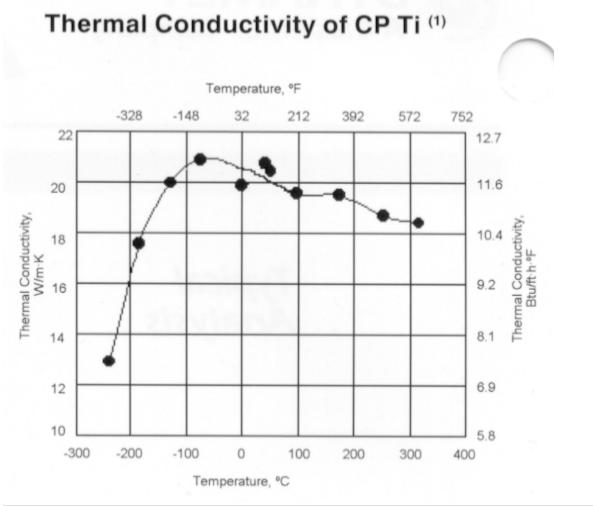
### CP Ti Grade 2: Erosion/Corrosion in Sea Water

Test Description	Flow Rate		Test	Erosion/Corrosion Rate		
Test Description	m/s	ft/s	Duration	mm/yr	mils/yr	
Brixham Sea, model condenser	9.8	32	12 months	0.003	0.12	
Kure Beach, NC, rotating disk	8.5	28	2 months	0.00013	0.005	
Kure Beach, NC, jet impingement	7.2	23.6	1 month	0.0005	0.02	
Wrightsville Beach, NC Micarta whi.	9	29.5	2 months	0.00018	0.007	
Lab test - no solids	7.2	23.6	10,000 hr	nil	nil	
Lab test - 40 g/l 60-mesh sand	2.0	6.5	2,000 hr	0.0025	0.1	
Lab test - 4% 80-mesh emery	4.1	13.5	17.5 hr	0.083	3.3	

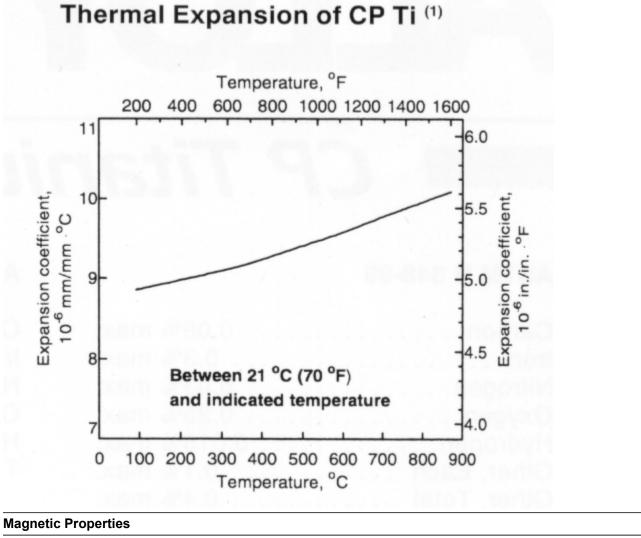
### CP Ti Grade 2: General Corrosion Rates in Various Media

Medium	Concentration	Tempo	erature	Corrosion Rate		
modium	%	°C	٩F	mm/yr	mils/yr	
Nitric Acid	35	boi	iling	0.127-0.508	5.0-20.0	
Nitric Acid + 0.01% K <sub>2</sub> Cr <sub>2</sub> O <sub>7</sub>	40	boi	boiling 0.01		0.39	
Ammonium Hydroxide	70	boiling		nil		
Stearic Acid	100	180	355	0.003	0.12	
Acetic Acid	0-99.5	boi	iling	nil		
Bismuth/lead	molten	300	570	<0.1	<4	
Bromine, moist	vapor	30	86	<0.003	0.12	
Hydrogen Peroxide, pH 4.3	5	66	150	0.061	2.4	
H_O_ + 20 g/I NaOH	10g/l	60 140		55.9	2200	

Properties					
Physical Properties					
Density	0.1630 lb/in <sup>3</sup>				
Mean Specific Heat (73°F)	0.1250 Btu/lb/°F				



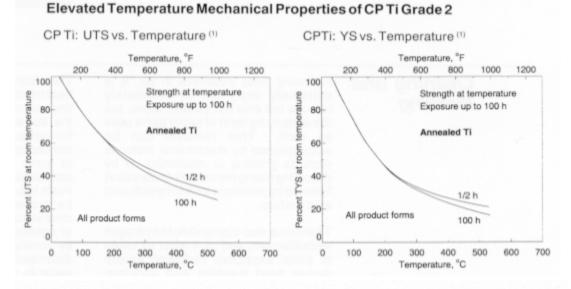
Modulus of Elasticity (E)	15.0 x 10 ₃ ksi
Beta Transus	1650 to 1700 °F
Alpha Transus	1610 to 1660 °F
Liquidus Temperature	3020 to 3040 °F
Electrical Resistivity	
Electrical resistivity	
104°F	294.8 ohm-cir-mil/ft
-	294.8 ohm-cir-mil/ft 367.0 ohm-cir-mil/ft



Magnetic Attraction

None

#### **Typical Mechanical Properties**



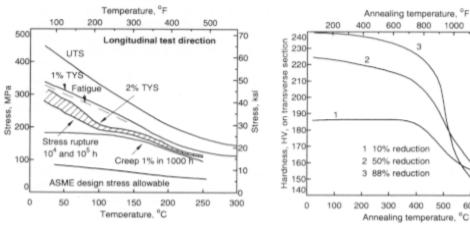
## **Fatigue Limits**

Approximate Fatigue Limit Range for CP	Ti Grade 2	
Smooth Axial Fatigue, R = 0.1	275-345 MPa	(40-50 ksi)

## Room Temperature Mechanical Properties of CP Ti Grade 2

	UTS	YS	%EI	%RA
Specified Minimum Properties	345 MPa (50 ksi)	275 MPa (40 ksi)	20	30
Typical Properties	510–605 MPa (74–88 ksi)	335–545 MPa (49–79 ksi)	21–29	47–54





Grade 2 Ti: Effect of Processing on Hardness (1)

600

300

400 500 600

800

1000

1200 1400

700 800

°C

## **Heat Treatment**

Heat treatments used for CP Ti are annealing and stress relieving. Annealing is used to fully soften the material and remove all residual stresses. Annealing of wrought products at typical temperatures (below the beta transus) results in a fully recrystallized

## **CP Titanium Grade 2**

equiaxed alpha structure. Precise control of grain size (and mechanical properties) can be achieved by adjusting the anneal temperature.

Stress relieving is used to remove some or most of the residual stresses from forming, or to recover compressive yield strength after stretching.

Titanium and its alloys have a high affinity for gases including oxygen, nitrogen and hydrogen. When CP Ti is heated in air, oxygen absorption results in the formation of an extremely hard, brittle, oxygen-stablized alpha phase layer known as alpha case.

Intermediate and final annealing of CP Ti is often performed in a vacuum or inert gas atmosphere to avoid alpha case formation and the associated material loss. Vacuum annealing can also be used to remove excess hydrogen pickup, a process known as vacuum degassing. Parts to be vacuum heat treated must be thoroughly cleaned (see Cleaning Notes).

### Typical Heat Treatments for CP Ti Grade 2

Anneal	595-705°C (1100-1300°F) 2 hrs-air cool (or equivalent)
Stress Relief	540-595°C (1000-1100°F) 15-30 min.—air cool (or equivalent)

## Workability

#### Hot Working

CP Ti Grade 2 can be processed by conventional techniques such as hot rolling, forging, and hot pressing. Temperatures for initial roughing may be as high as 30-50°C (50-100°F) above the beta transus, and temperatures for finish processing are typically in the alpha/beta phase field, ranging from about 815°C (1500°F) to about 900°C (1650°F).

CP Ti Grade 2 can be formed by standard methods such as hot rolling, forging, spin forming, hydroforming, and hot pressing. Typically, more severe forming is done in the temperature range of 480-540°C (900-1000°F) and milder forming from 200-315°C (400-600°F). Care must be taken to prevent the formation of excessive alpha case, and alpha case must be removed after processing.

#### Cold Working

CP Ti Grade 2 has good ductility and can be formed at room temperature by various standard methods including bending, stretch forming, heading, stamping, and drawing. CP Ti work hardens fairly rapidly, which is a limitation in some operations, such as cold drawing. The Bauschinger effect results in a drop of up to 25% in compressive yield strength upon stretching at room temperature; this drop can be recovered by stress relieving. Due to the low modulus of titanium, springback allowances are significant. Hot sizing after cold forming is often used to correct for variations in springback.

#### Machinability

The machining characteristics of CP Ti Grade 2 are similar to those of austenitic stainless steels. In general, low cutting speeds, heavy feed rates, and copious amounts of cutting fluid are recommended. Sharp tools and rigid setups are also important. Because of the strong tendency of titanium to gall and smear, feeding should never be stopped while the tool and workpiece are in moving contact. Non-chlorinated cutting fluids are generally used to eliminate any possibility of chloride-induced stress-corrosion cracking. It should be noted that titanium chips are highly combustible and appropriate safety precautions are necessary.

Following are typical feeds and speeds for CP Ti Grade 2.

## Typical Machining Speeds and Feeds – Titanium Alloy CP Titanium Grade 2

The speeds and feeds in the following charts are conservative recommendations for initial setup. Higher speeds and feeds may be attainable depending on machining environment.

## Turning-Single-point and Box Tools

Depth	High Speed Tools						
of Cut	Tool			Tool	Speed (fpm)		Feed
(Inches)	Material	Speed (fpm)	Feed (ipr)	Material	Uncoated	Coated	(ipr)
.150	T15, M42	105	.010	C2	250	320	.008
.025		115	.005	C3	290	370	.005

#### Turning—Cut-Off and Form Tools

Tool N	laterial		Feed (ipr)						
High	Car-	Speed	Cut-C	Off Tool Wid	th (Inches)		Form Too	Width (Inc	hes)
Speed Tools	bide Tools	(fpm)	1/16	1/8	1/4	1/2	1	1 ½	2
T15,		80	.001	.0015	.002	.0025	.0015	.001	.001
M42	C2	185	.001	.0015	.002	.0025	.0015	.001	.001

#### Rough Reaming

High Speed		Carbide	e Tools	Feed (ipr) Reamer Diameter (Inches)					
Tool Material	Speed (fpm)	Tool Material	Speed (fpm)	1/8	1/4	1/2	1	1 ½	2
M1, M2, M7	120	C2	300	.004	.008	.012	.018	.022	.025

#### Drilling

High Speed Tools										
Tool	Speed		Feed (inches per revolution) Nominal Hole Diameter (inches)							
Material	(fpm)	1/16	1/8	1/4	1/2	3/4	1	1 ½	2	
M10, M7, M1	40-55	.001	.002	.005	.008	.010	.012	.025	.017	

#### Die Threading

FPM for High Speed Tools						
Tool Material	7 or less, tpi	8 to 15, tpi	16 to 24, tpi	25 and up, tpi		
M1, M2, M7, M10	5-20	9-25	10-30	15-40		

#### Milling, End-Peripheral

Depth		Н	High Speed Tools					Carbide Tools				
of Cut	Tool	Speed	Feed (ipt) Cutter Diameter (in)			Tool	Speed	Feed (	ipt) Cutte	er Diame	eter (in)	
(inches)	Material	(fpm)	1/4	1/2	3/4	1-2	Material	(fpm)	1/4	1/2	3/4	1-2
.050	M2, M3 M7	130	.002	.003	.005	.006	C2	323	.002	.003	.006	.008

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#### Broaching

- opping						
High Sp	eed Tools	High Speed Tools				
Tool Material	Speed (fpm)		Tool Material	Speed (fpm)	Chip Load (ipt)	
M1, M7, M10 Nitrited	12-40		M2, M7	25	.003	

When using carbide tools, surface speed feet/minute (SFPM) can be increased between 2 and 3 times over the high-speed suggestions. Feeds can be increased between 50 and 100%.

Figures used for all metal removal operations covered are average. On certain work, the nature of the part may require adjustment of speeds and feeds. Each job has to be developed for best production results with optimum tool life. Speeds or feeds should be increased or decreased in small steps.

## Typical Minimum Stock Removal Requirements for Ti and Ti Alloys (after Thermal Exposure in Air)

Heat Treatment	Thermal Cycle	Removal Required
Anneal	705°C (1300°F) 2 hrs.	0.020 mm (0.0008 in.)
Stress Relief	540-595°C (1000-1100°F) 30 min	0.005 mm (0.0002 in.)

Weldability

CP Ti Grade 2 can be welded using CP Ti filler metal. Inert gas shielding techniques must be employed to prevent oxygen pickup and embrittlement in the weld area. Gas tungsten arc welding is the most common welding process for CP Ti. Gas metal arc welding is used for thick sections. Plasma arc welding, spot welding, electron beam, laser beam, resistance welding, and diffusion welding have all been used successfully in CP Ti welding applications.

## Other Information

#### Wear Resistance

Commercially pure Ti has a tendency to gall and is not recommended for wear applications.

#### **Descaling (Cleaning)**

Following heat treatment in air, it is extremely important to completely remove not only the surface scale, but the underlying layer of brittle alpha case as well. This removal can be accomplished by mechanical methods such as grinding or machining, or by descaling (using molten salt or abrasive) followed by pickling in a nitric/hydroflouric acid mixture.

Titanium is also susceptible to hydrogen embrittlement, and care must be taken to avoid excessive hydrogen pickup during heat treating and pickling/chemical milling.

Final heat treatments on finished parts must be performed in vacuum if machining or pickling is to be avoided.

The cleanliness of parts to be vacuum heat treated is of prime importance. Oils, fingerprints, or residues remaining on the surface can result in alpha case formation, even in the vacuum atmosphere. In addition, chlorides found in some cleaning agents have been associated with SCC of titanium alloys. Parts to be vacuum heat treated should be processed as follows: thorough cleaning using a non-chlorinated solvent or aqueous cleaning solution, followed by rinsing with copious quantities of deionized or distilled (not regular tap) water to remove all traces of cleaning agent, and finally, drying. Following cleaning, parts must be handled with clean gloves to prevent recontamination of the surface.

#### **Applicable Specifications**

- AMS 4902 (Sheet, Strip, Plate)
- AMS 4942 (Seamless Tubing)
- ASTM B265 (Sheet, Strip, Plate)
- ASTM B367 (Castings)

- AMS 4941 (Welded Tubing)
   AMS 4951 (Weld Filler Metal Wire)
   ASTM B249 (Ber Biller)
- ASTM B348 (Bar, Billet)
- ASTM F67 (Unalloyed Ti for Surgical Implants)

# AWS A5.16-70 (Weld Filler Metal Wire and Rod) Forms Manufactured

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Bar-Rounds	<ul> <li>Bar-Shapes</li> </ul>
Dynalube Coil	• Ingot
• Plate	Sheet
SMART Coil     Titanium Coil	<ul> <li>ULTRABAR® Precision Bar</li> </ul>
Weld Wire	• Wire
Wire-Shapes	

#### References

The information in this publication was compiled from a variety of sources, including the following:

Materials Properties Handbook: Titanium Alloys, ASM International, 1994 Aerospace Structural Metals Handbook, Volume 4, CINDAS/Purdue University, 1998 Titanium: a Technical Guide, ASM International, 1988

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Metals Handbook, Desk Edition, ASM International, 1984 Specifications Book, International Titanium Association, 1999 Metcut Research Associates Inc. data

Dynamet technical papers and unpublished data

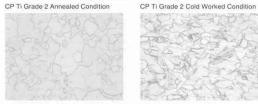
#### **Technical Articles**

New, Precision Titanium ULTRABAR™ for Screw Machining Medical and Other Precision Parts

CP Ti Grade 2 specimens can be prepared for metallographic examination by standard methods. Abrasive cutting, especially of small samples, is not recommended due to the tendency to "burn" the surface and produce alpha case. Kroll's reagent (1–3% hydroflouric acid plus 2–6% nitric acid in water) is

commonly used for determination of general microstructure. Oxygen contamination in CP Ti cannot be reliably detected by metallography: its presence must be determined by microhardness testing. Some typical microstructures are illustrated below.

#### Microstructures of CP Ti Grade 2 (approximate magnification 200X)



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